

# **SIMULATION OF THE CONCRETE CHLORIDE NT BUILD-492 MIGRATION TEST**

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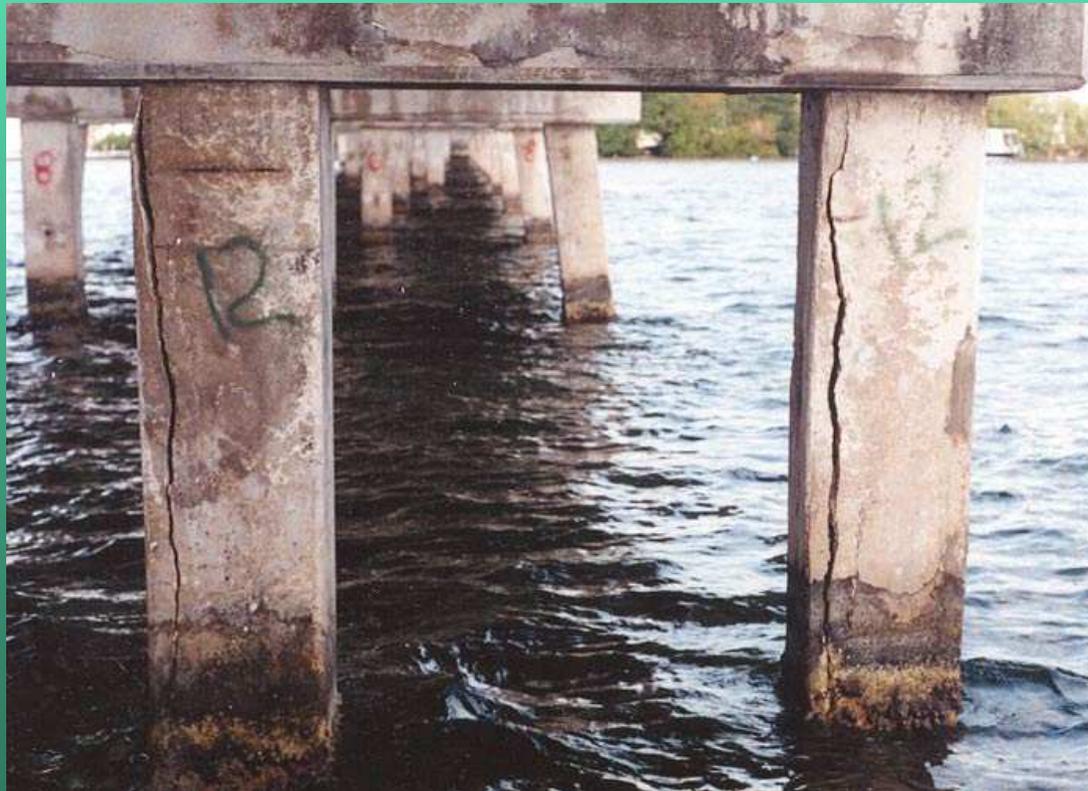


# Contents

- Nordtest 492 experiment
- Electro-diffusion model
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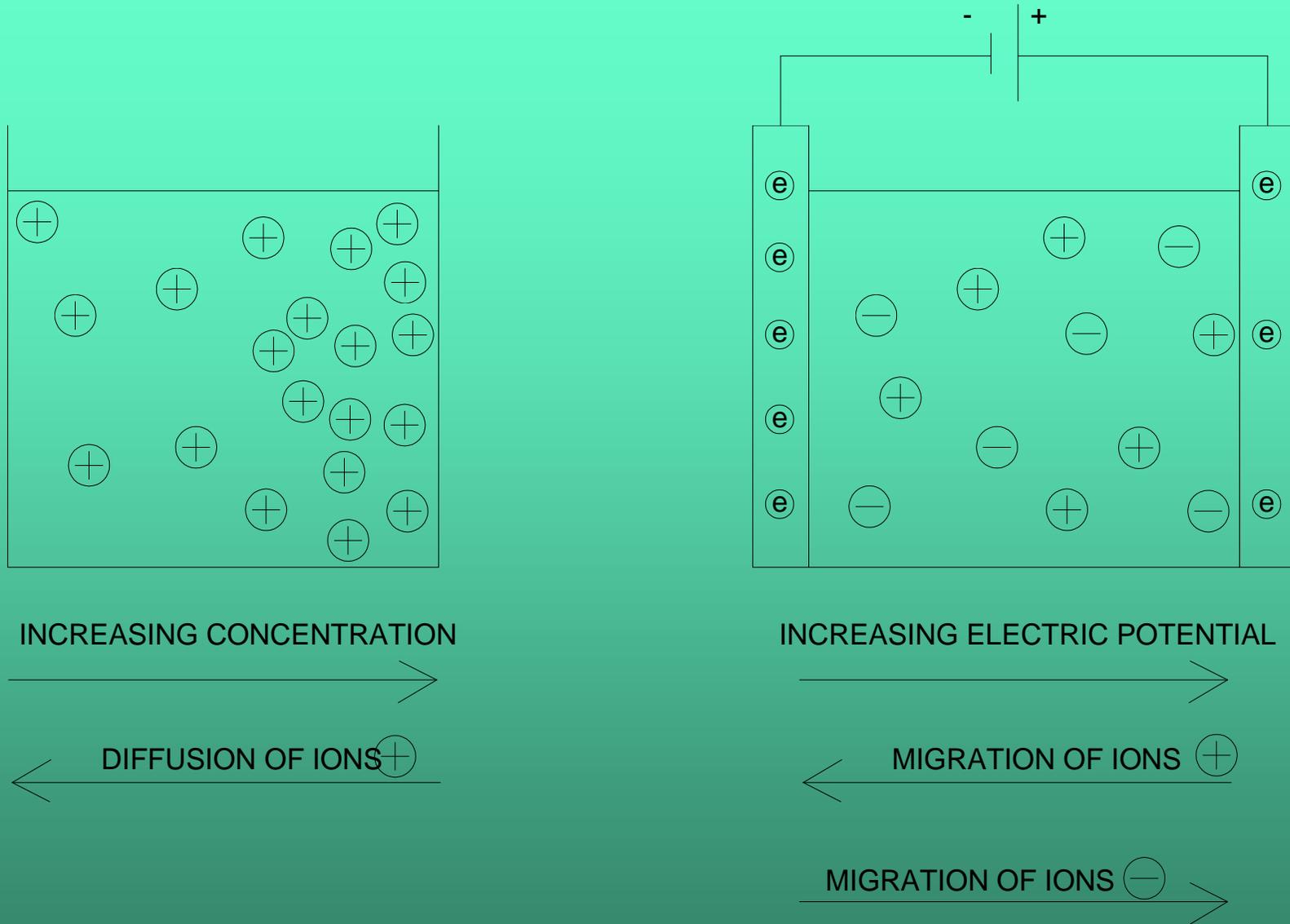
## **Justification**

- **Corrosion of steel reinforced concrete is caused by chloride ingress**
- **Widespread occurrence and high cost of repair.**



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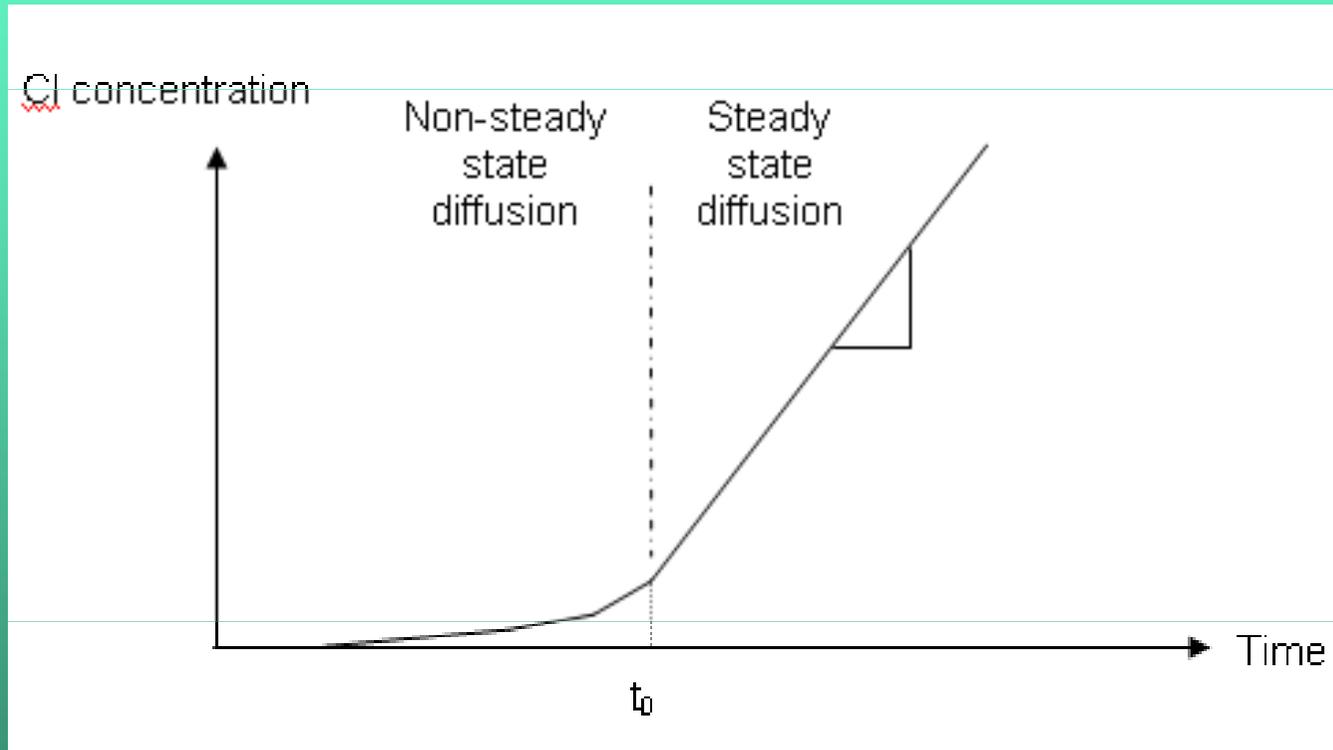


**Schematic representation of the ionic diffusion and migration processes (Bockris and Reddy 1998)**

# •Fick's laws

$$J_i = D_i \frac{\partial c_i}{\partial x}$$

$$\frac{\partial C_i}{\partial t} = D_i \frac{\partial^2 C_i}{\partial x^2}$$



$J_i$ = flux of species  $i$  [mol/m<sup>2</sup>/s]

$D_i$ = diffusion coefficient of  $i$  [m<sup>2</sup>/s]

$c_i$ = ionic concentration of  $i$  in the pore fluid [mol/m<sup>3</sup>]

$x$ = distance [m]

# •Nernst-Planck equation

$$J_i = \underbrace{D_i \frac{\partial c_i}{\partial x}}_{\text{Diffusion term}} + \underbrace{\frac{z_i F}{RT} D_i c_i \frac{\partial E}{\partial x}}_{\text{Migration term}}$$

$$c(x, t) = \frac{c_s}{2} \left[ e^{ax} \operatorname{erfcf} \left( \frac{x + aDt}{2\sqrt{Dt}} \right) + \operatorname{erfcf} \left( \frac{x - aDt}{2\sqrt{Dt}} \right) \right]$$

$$a = zFE/RT$$

$J_i$ = flux of species  $i$  [mol/m<sup>2</sup>/s]

$D_i$ = diffusion coefficient of  $i$  [m<sup>2</sup>/s]

$c_i$ = ionic concentration of  $i$  in the pore fluid [mol/m<sup>3</sup>]

$x$ = distance [m]

$z_i$ = electrical charge of  $i$ ,

$F$ = Faraday constant [Coulomb/mol]

$R$ = gas constant [J/mol/°K]

$T$ = absolute temperature [°K]

$E$ = electrical potential [V].

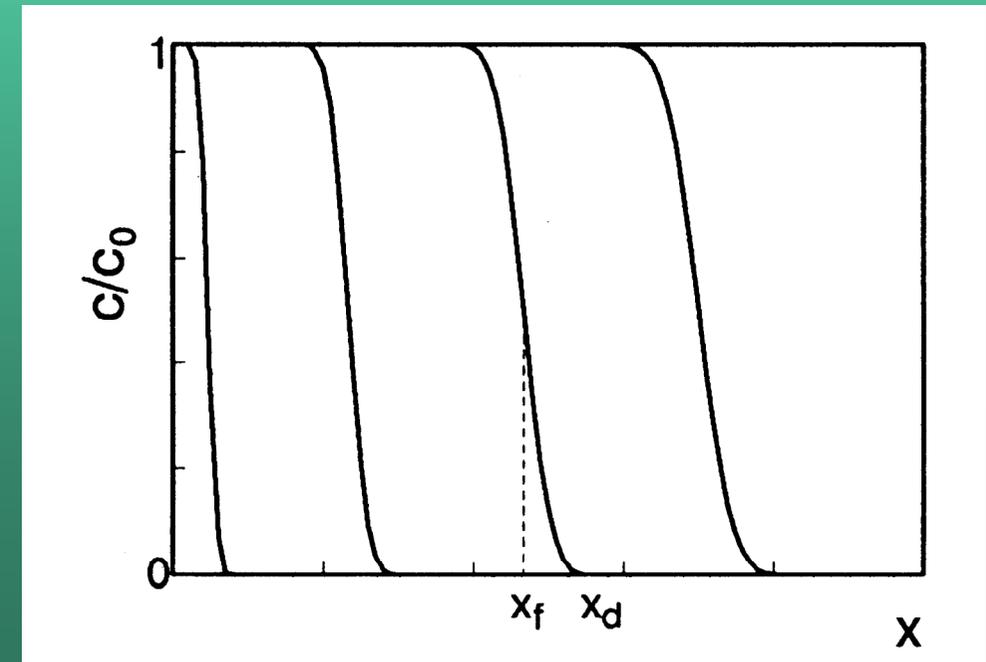
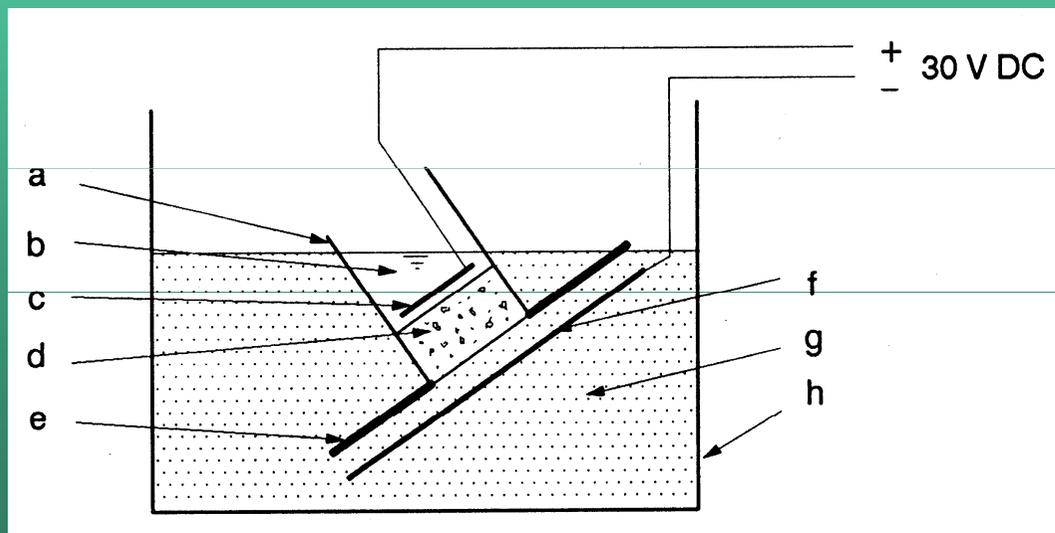
ACI MATERIALS JOURNAL

TECHNICAL PAPER

Title no. 89-M6

## Rapid Determination of the Chloride Diffusivity in Concrete by Applying an Electrical Field

by Tang Luping and Lars-Olof Nilsson



## nordtest method

NT BUILD 492

Approved 1999–11

1(8)

**CONCRETE, MORTAR AND CEMENT-BASED REPAIR MATERIALS:  
CHLORIDE MIGRATION COEFFICIENT FROM  
NON-STEADY-STATE MIGRATION EXPERIMENTS**

UDC 691.32/691.53/691.54

Key words: Chlorides, concrete, diffusion, mortar, repair materials, migration, test method

### 1 SCOPE

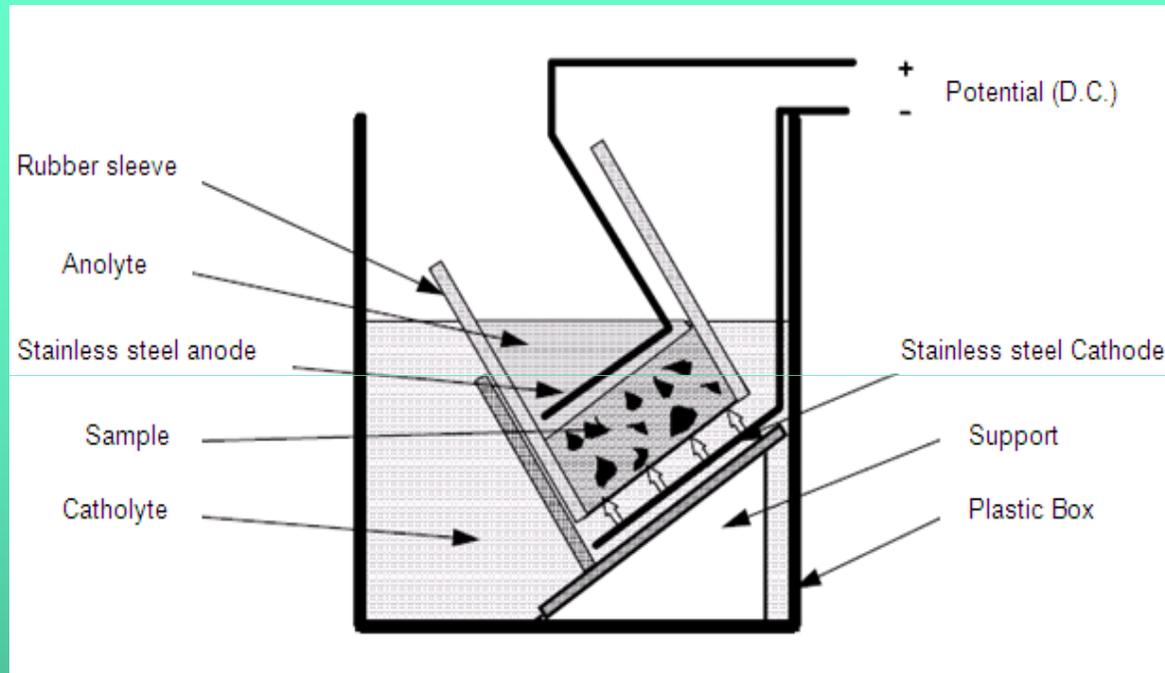
This procedure is for determination of the chloride migration coefficient in concrete, mortar or cement-based repair materials from non-steady-state migration experiments.

### 5 SAMPLING

The method requires cylindrical specimens with a diameter of 100 mm and a thickness of 50 mm, sliced from cast cylinders or drilled cores with a minimum length of 100 mm. The cylinders and cores should meet the requirements described

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- $D_{nssm}$ : non-steady-state migration coefficient,  $m^2/s$ ;
- $z$ : absolute value of ion valence, for chloride,  $z = 1$ ;
- $F$ : Faraday constant,  $F = 9.648 \times 10^4 \text{ J/(V}\cdot\text{mol)}$ ;
- $U$ : absolute value of the applied voltage,  $V$ ;
- $R$ : gas constant,  $R = 8.314 \text{ J/(K}\cdot\text{mol)}$ ;
- $T$ : average value of the initial and final temperatures in the anolyte solution,  $K$ ;
- $L$ : thickness of the specimen,  $m$ ;
- $x_d$ : average value of the penetration depths,  $m$ ;
- $t$ : test duration, seconds;
- $\text{erf}^{-1}$ : inverse of error function;
- $c_d$ : chloride concentration at which the colour changes,  $c_d = 0.07 \text{ N}$  for OPC concrete;
- $c_0$ : chloride concentration in the catholyte solution,  $c_0 = 2 \text{ N}$ .



$$D_{nssm} = \frac{RT}{zFE} \cdot \frac{x_d - \alpha\sqrt{x_d}}{t}$$

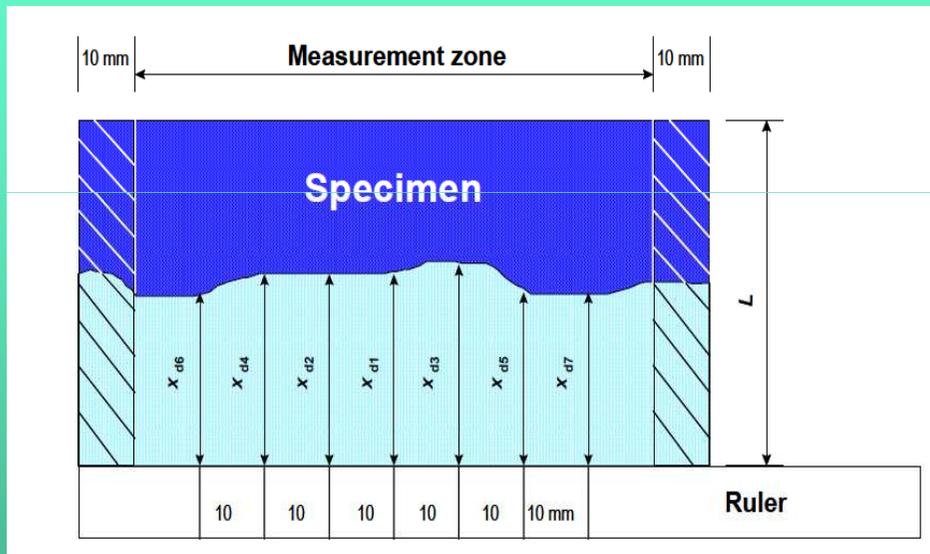
where:

$$E = \frac{U - 2}{L}$$

$$\alpha = 2 \sqrt{\frac{RT}{zFE}} \cdot \text{erf}^{-1} \left( 1 - \frac{2c_d}{c_0} \right)$$

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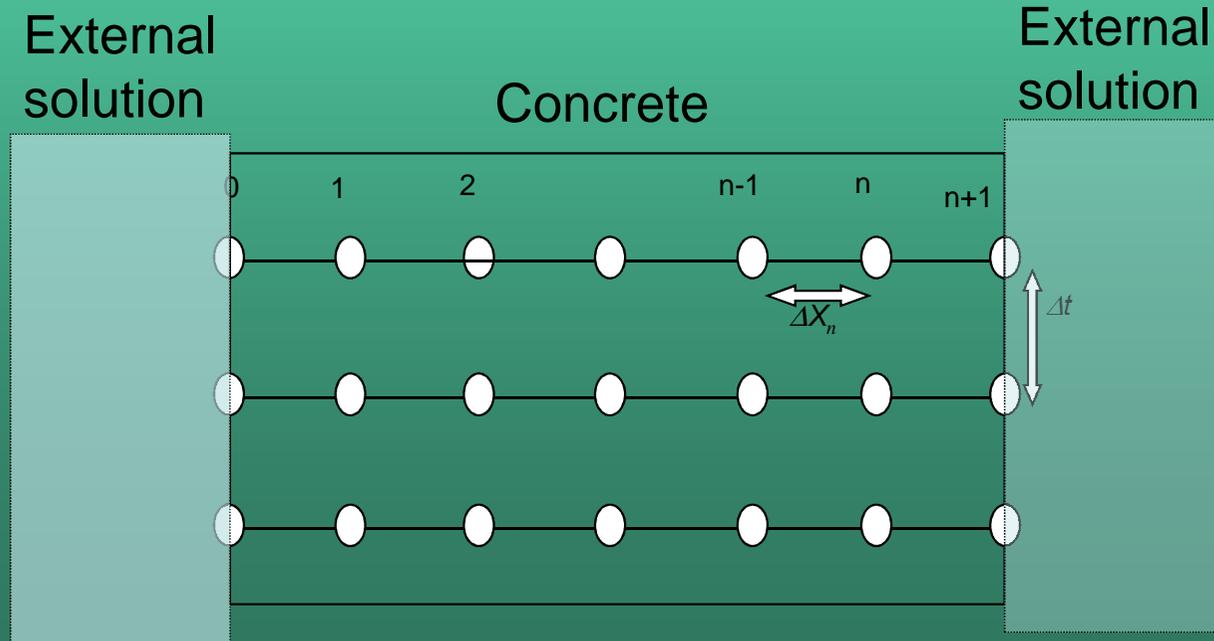
chloride penetration depths after applying 0.1 N silver nitrate in a chloride contaminated concrete sample

## Electro-diffusion model for chlorides in concrete

- Nernst-Planck equation:

$$J_i = \underbrace{D_i \frac{\partial c_i}{\partial x}}_{\text{Diffusion}} + \underbrace{\frac{z_i F}{RT} D_i c_i \left( \frac{\partial E}{\partial x} \right)}_{\text{Migration}}$$

- Charge electroneutrality (Kirchoff's law):  $0 = F \sum_i z_i J_i$



## Definitions

- Multi-species
- Binding Capacity
- Pore Solution concentration

## Definitions

$C_l$  : free ions per unit volume of liquid

$C_s$ : total ions per unit volume of the solid

$\alpha$ : binding capacity factor

$\varepsilon$ : porosity

$$\alpha = \frac{C_s}{C_l}$$

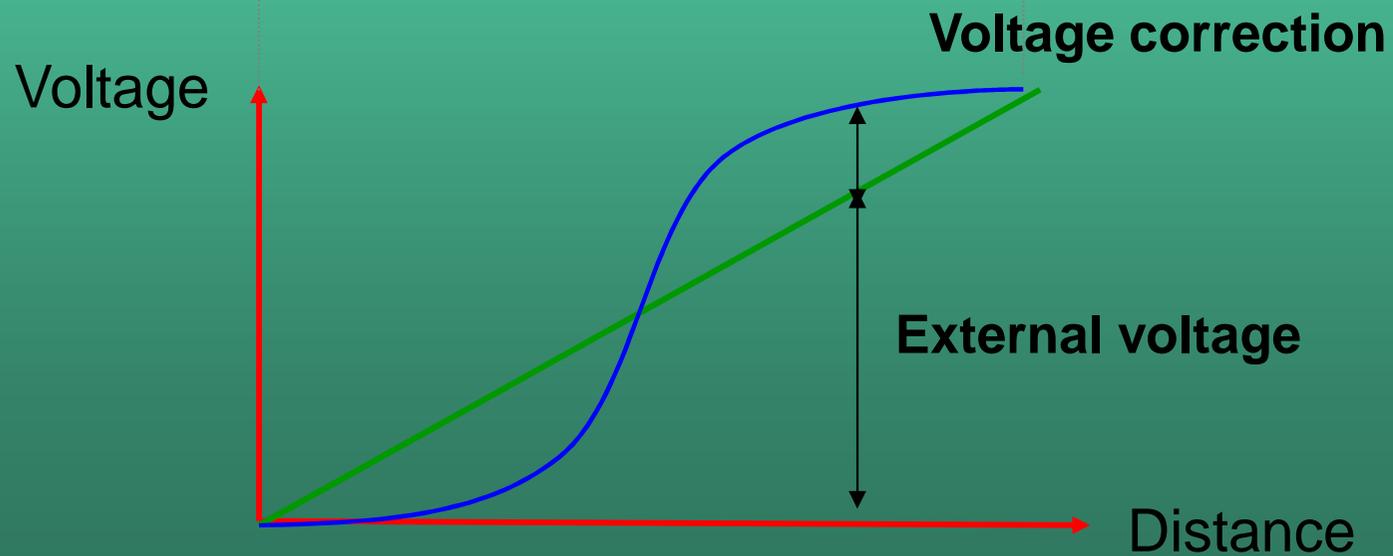
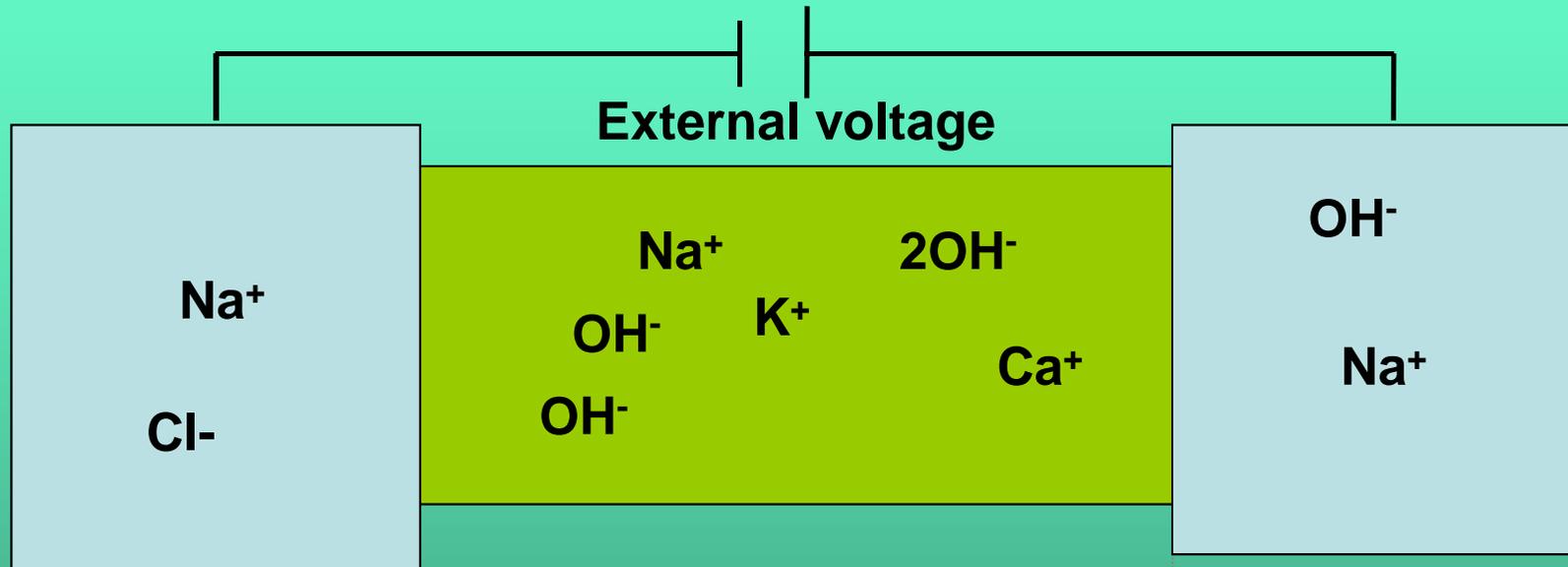
$F = D_{app} \frac{dC_s}{dx}$  The flux is calculated per unit area of the porous material and the average concentration in the material

$F = \varepsilon D_i \frac{dC_l}{dx}$  The flux is calculated per unit cross-sectional area of the pores and the concentration in the free liquid

$$\frac{\alpha}{\varepsilon} = \frac{D_i}{D_{app}}$$

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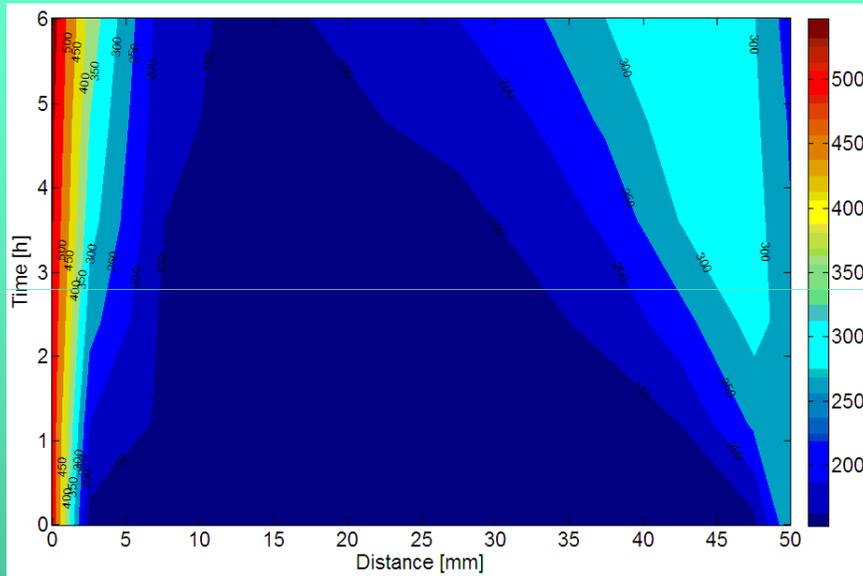
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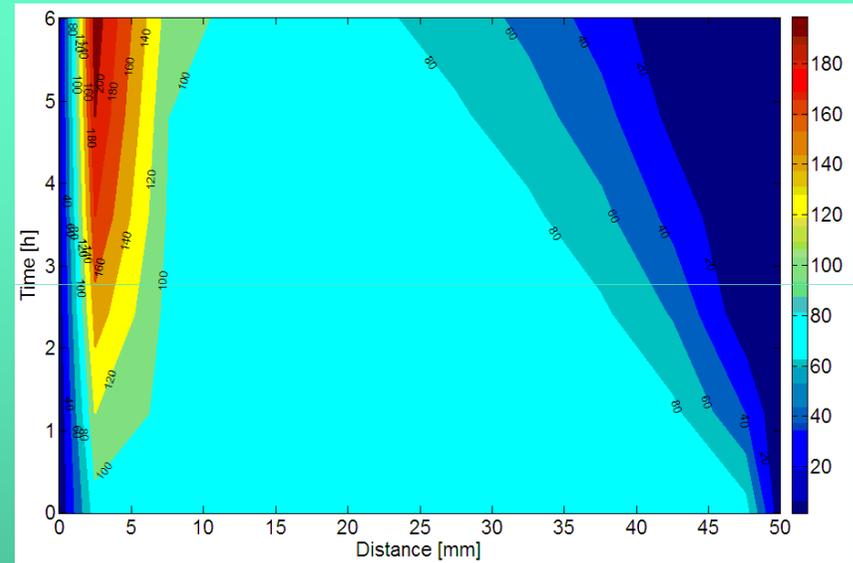
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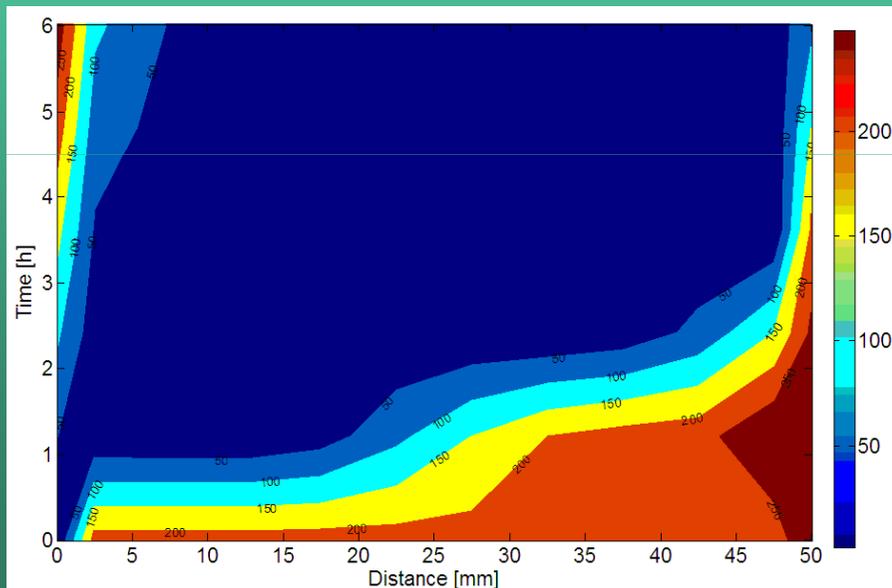
## Numerical Model



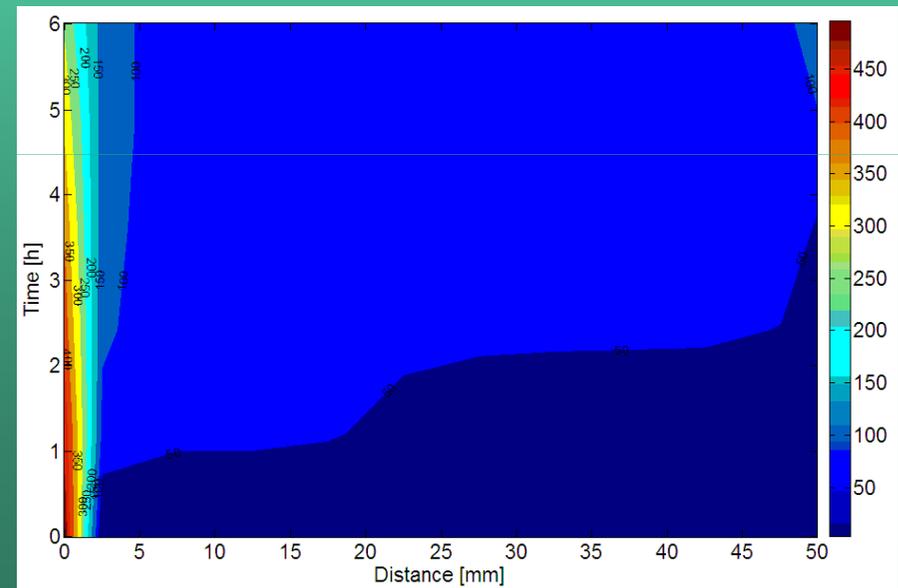
Concentration Na [mol/m<sup>3</sup>]



Concentration K [mol/m<sup>3</sup>]

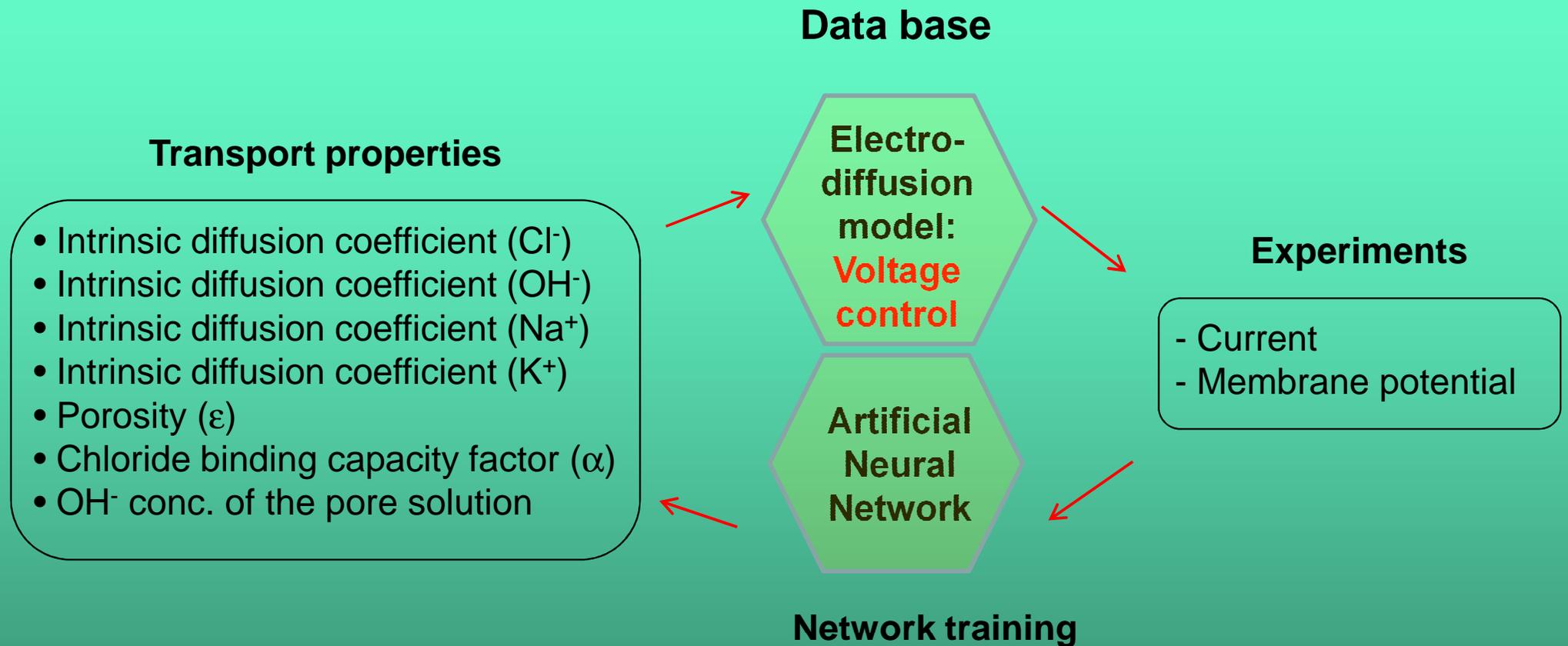


Concentration OH [mol/m<sup>3</sup>]



Concentration Cl [mol/m<sup>3</sup>]

# Optimization Model



## References

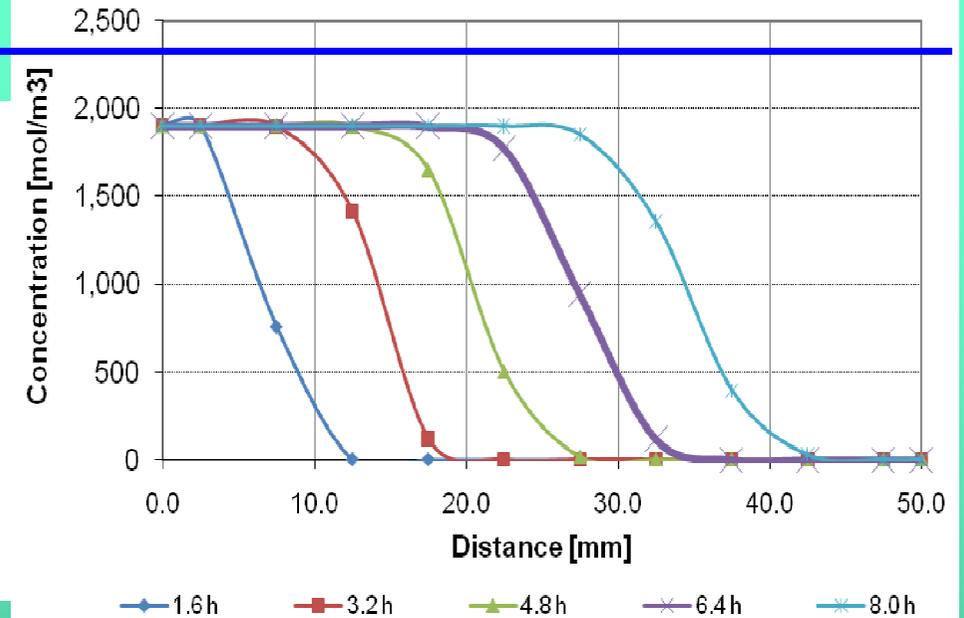
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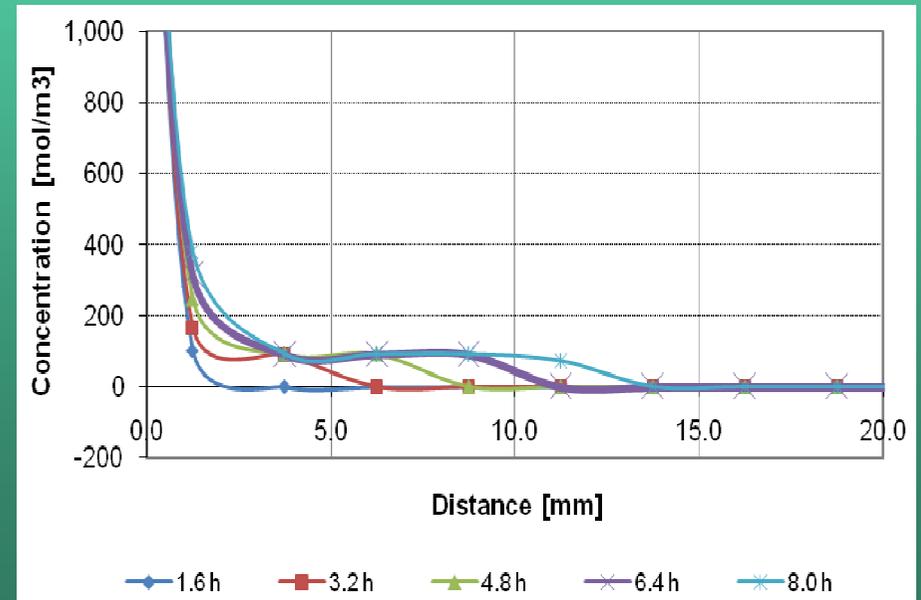
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	Valence	Intrinsic Diffusion D m <sup>2</sup> /s	Concentration [mol/m <sup>3</sup> ] (in liquid)			Capacity factor
			negative	in sample	positive	
Chloride	-1	1.90 × 10 <sup>-10</sup>	1900	0.00E+00	0	1
No of cells:	500		Sample length [m]	0.05		
Voltage correction?	<b>NO</b>		Sample radius [m]	0.05		
Time step [s]:	1		Room temp [K]	295		
Run time [hours]:	8		Cell volumes [m <sup>3</sup> ]:	1		
Porosity:	1		Heat loss fact [J/K]:	0.3		
Applied voltage [V]:	8					

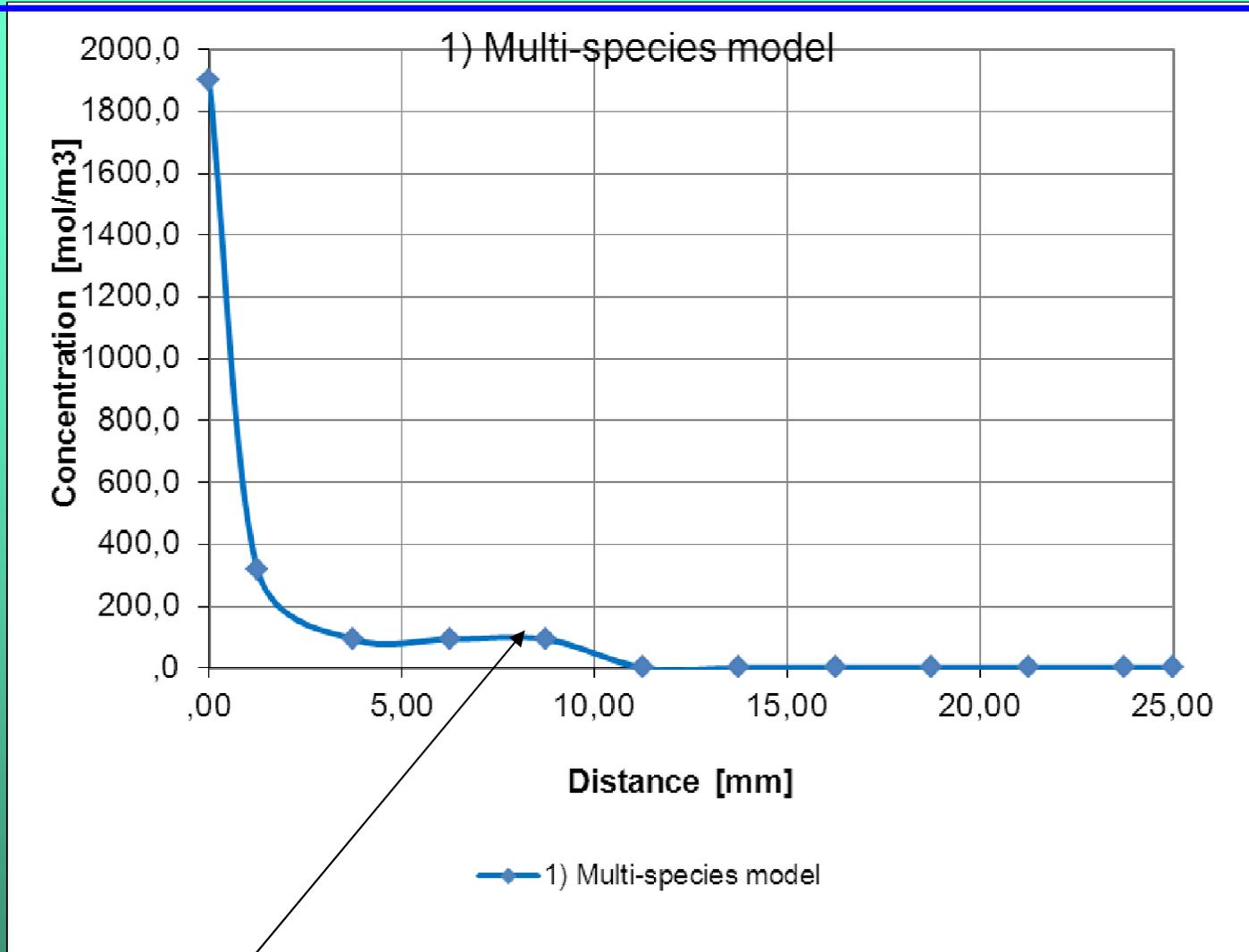


	Valence	Intrinsic Diffusion D m <sup>2</sup> /s	Concentration [mol/m <sup>3</sup> ] (in liquid)			Capacity factor
			negative	in sample	positive	
hydroxyl	-1	7.877E-11	0	239.973	300	0.171
chloride	-1	1.904E-10	1900	0.00E+00	0	0.383
sodium	1	2.061E-11	1900	7.92E+01	300	0.171
potassium	1	4.099E-12	0	1.61E+02	0	0.171
No of cells:	500		Sample length [m]	0.05		
Voltage correction?	<b>YES</b>		Sample radius [m]	0.05		
Time step [s]:	1		Room temperature [K]	295		
Run time [hours]:	8		Cell volumes [m <sup>3</sup> ]:	0.03		
Porosity:	0.171		Heat loss factor [J/K]:	0.30		
Applied voltage [V]:	8					



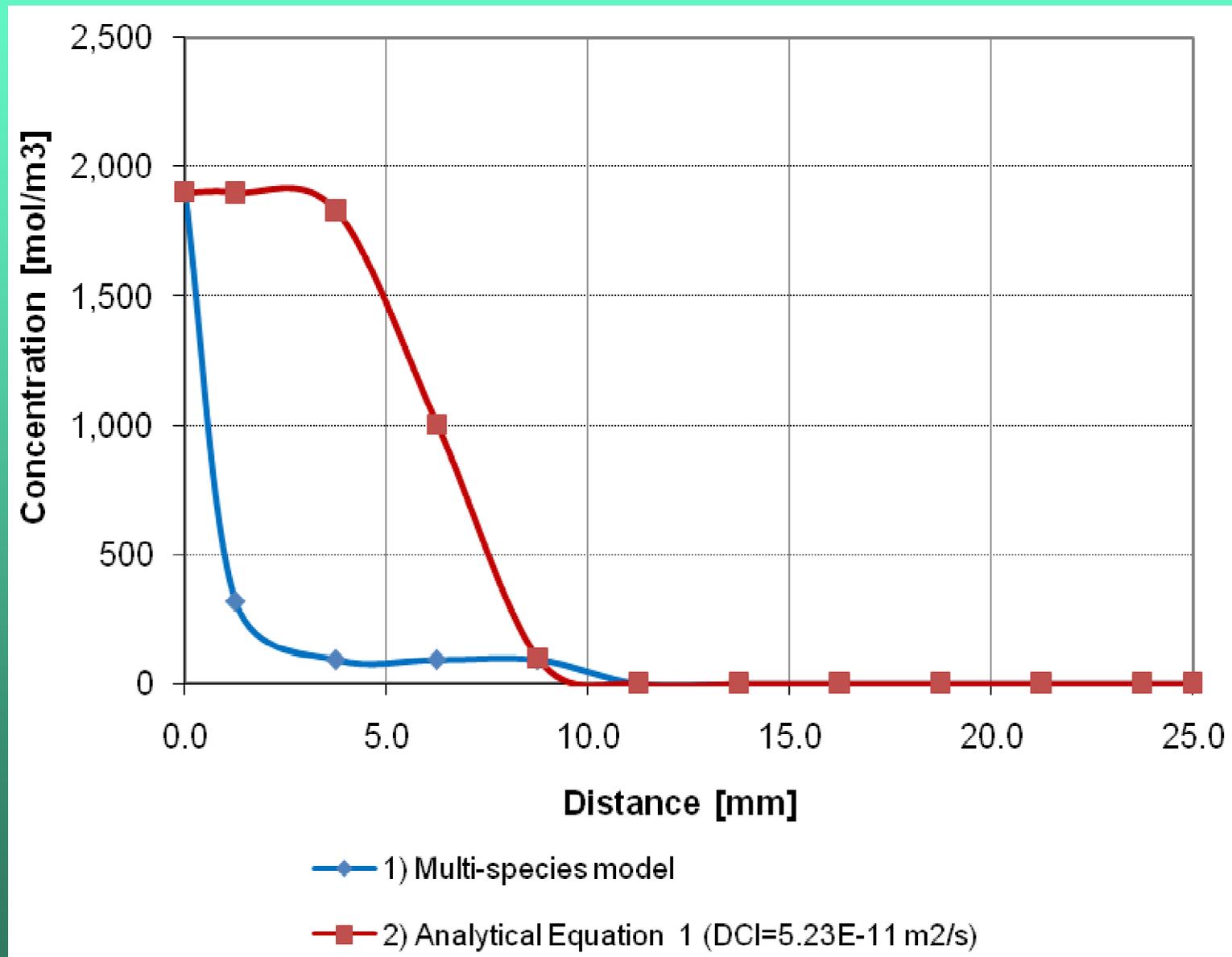
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chloride profile at 6.4 hours had a penetration of 9.3 mm when the concentration was 70 mol/m<sup>3</sup>

The chloride profile at 6.4 hours had a penetration of 9.3 mm when the concentration was 70 mol/m<sup>3</sup>



Thanks